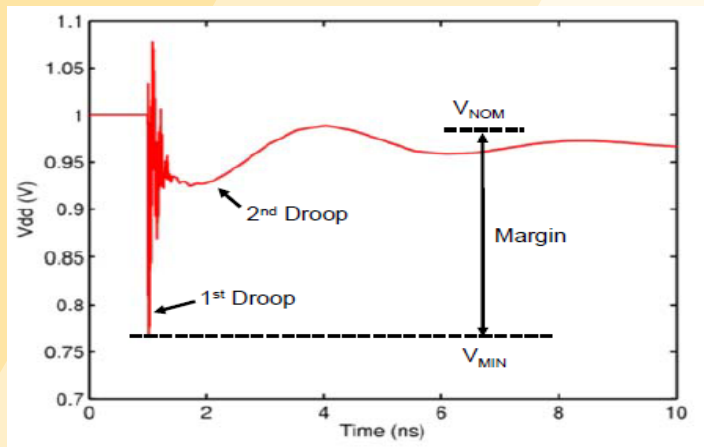


Analysis of Maximum Voltage Droops In Power Delivery Network

Students : Seunghyup Han
Faculty : Prof. Madhavan Swaminathan

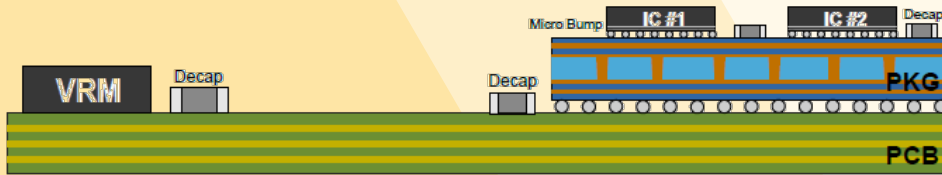
- Identify voltage droops in an efficient way
- The ways to effectively analyze and clarify the causes of voltage droops
- Estimate voltage droops from a step current considering its rise time
- Estimate voltage droops from a step current when multiple impedance peaks existed



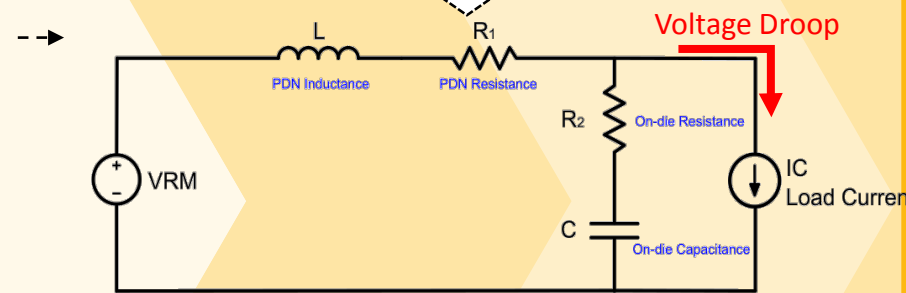
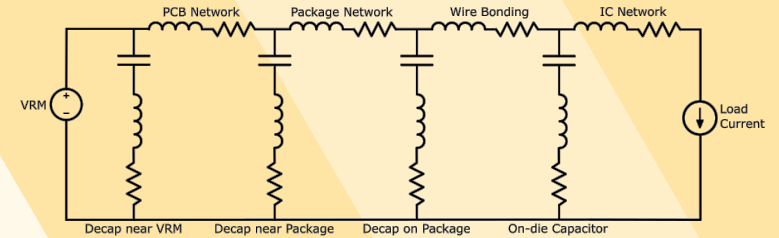
Voltage noise waveform and associated worst-case voltage margin. [Courtesy : P. N. Whatmough et al, 2015]

2.1 Simplified Equations to Predict Maximum Voltage Droops

- Based Assumption for PDN



[Typical PDN model of the high-performance computing system consisting of PCB, package, and ICs]



Simplified PDN circuit based on the assumption [Modified from L.Smith et al, 2018]

- Simplified equations to predict voltage droops [L.Smith et al, 2018]

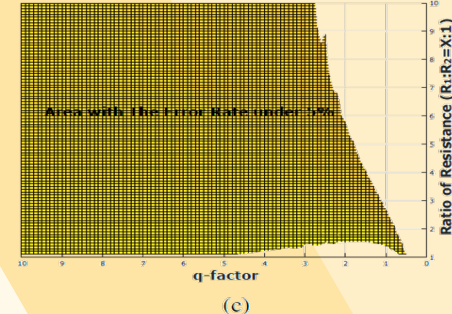
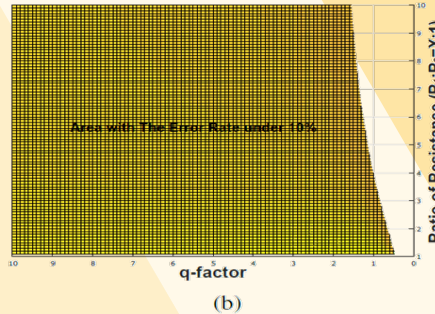
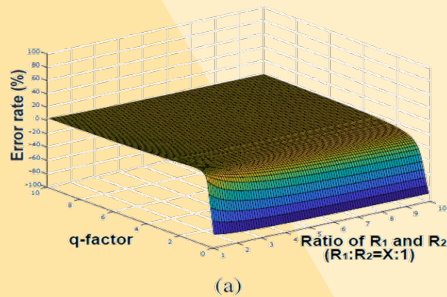
$$V_{impulse} = \frac{1}{C} \cdot \frac{I_{avg}}{f_{clk}} \quad : \text{Maximum voltage droop from impulse current}$$

$$V_{step} = Z_0 \cdot I_{step} \quad : \text{Maximum voltage droop from step current}$$

$$V_{resonance} = Z_{peak} \cdot \frac{4}{\pi} \cdot I_{resonance} \quad : \text{Peak to peak voltage ripple from resonant current}$$

- Voltage droops from a step current

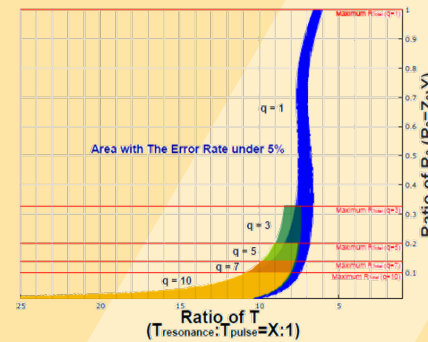
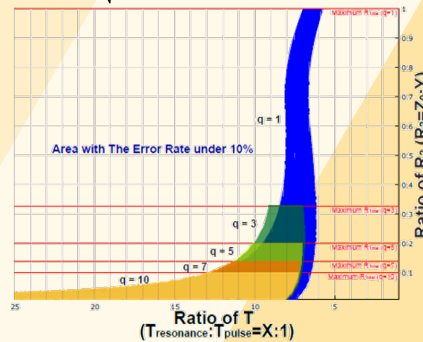
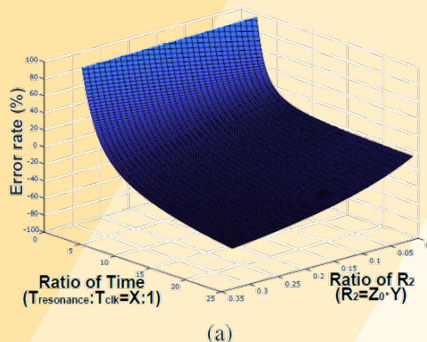
$$v(t)_{step} = R_1 + Z_0 \cdot e^{-\left(\frac{2\pi f_0}{2Q}\right) \cdot t} \cdot \frac{(R_2 - R_1)}{\sqrt{(R_2 - R_1)^2}} \cdot \frac{\left(1 - \frac{1}{Q^2} \frac{R_1 R_2}{(R_1 + R_2)^2}\right)^2}{1 - \frac{1}{4Q^2}} \cdot \cos\left(2\pi f_0 \cdot \sqrt{1 - \frac{1}{4Q^2}} \cdot t - \varphi\right)$$



[Error rates in the calculated voltage droops from a step current depending Q and the ratio of R1 to R2]

- Voltage droops from an impulse current

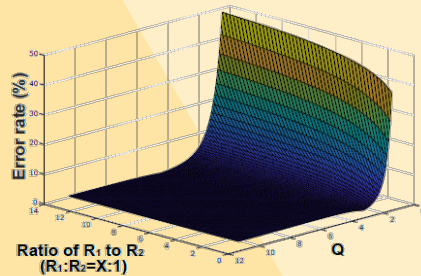
$$v(t)_{impulse} = R_2 \cdot \delta(0) + \frac{1}{C} \cdot e^{-\left(\frac{2\pi f_0}{2Q}\right) \cdot t} \cdot \frac{\left(1 - \frac{1}{Q^2} \frac{R_1 R_2}{(R_1 + R_2)^2}\right)^2}{1 - \frac{1}{4Q^2}} \cdot \cos\left(2\pi f_0 \cdot \sqrt{1 - \frac{1}{4Q^2}} \cdot t - \varphi\right)$$



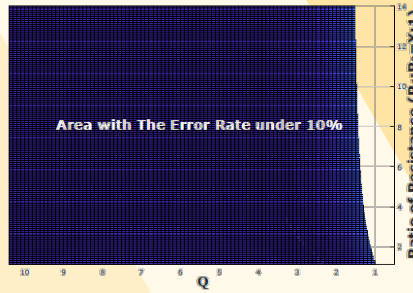
[Error rates in calculated voltage droops from a rectangular shaped impulse current depending on the ratio of resonance period to pulse time duration, and the ratio of R2 resistance with respect to Z0]

- Voltage droops from a resonant current**

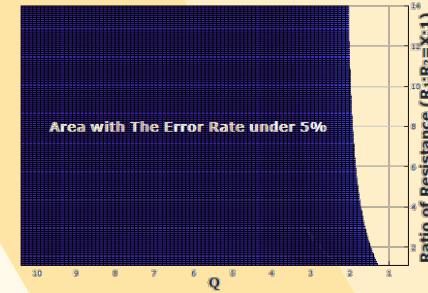
$$Z_{f_0} = Z_{peak} + \frac{R_1 R_2}{R_1 + R_2} + j \cdot Q(-R_1 + R_2)$$



(a)



(b)



(c)

[Error rates in the calculated voltage droops from a resonant current depending Q and the ratio of R1 to R2.]

- Sufficient Condition for the reliable voltage droop results**

- The equation for voltage response to a step current

- : Q needs to be higher than 3

- : If Q is less than 2, the ratio resistance needs to be considered

- The equation for voltage response to an impulse current

- : Pulse time duration and R_2 need to be closed to zero

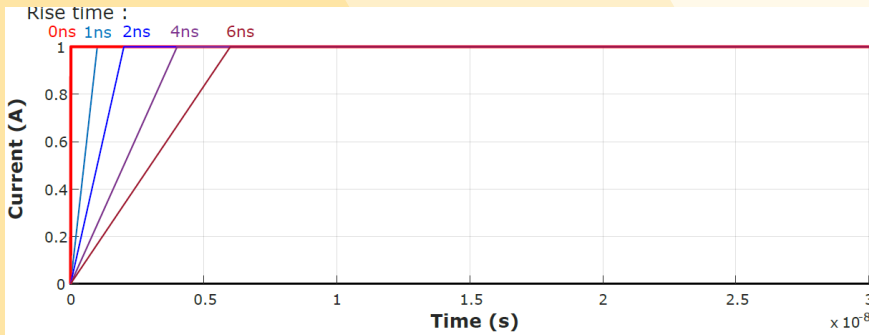
- : Pulse time duration needs to be at least 7:1

- The equation for voltage response to a resonant current

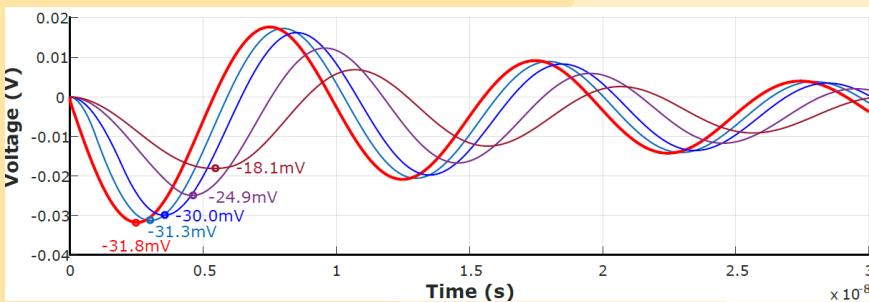
- : Q needs to be higher than 2

3.1 Step Current with Rise Time

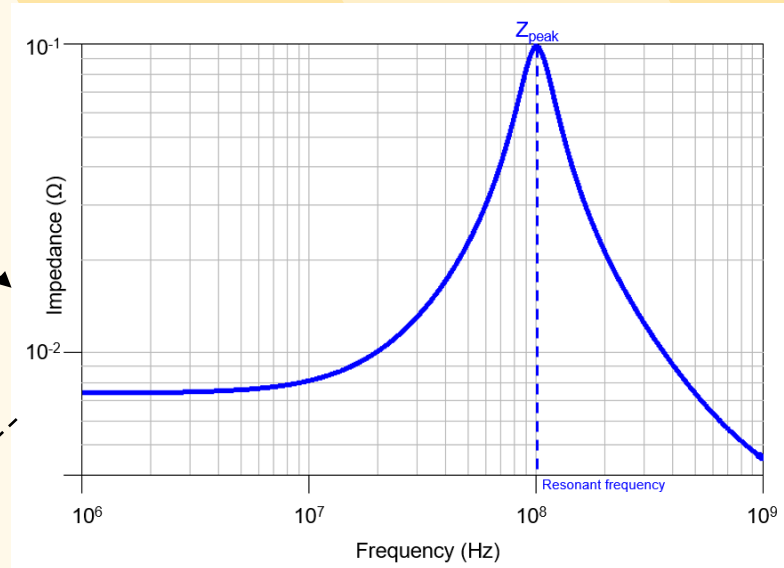
- Voltage droops from a step current with different rise times



[Step current with different rise times]



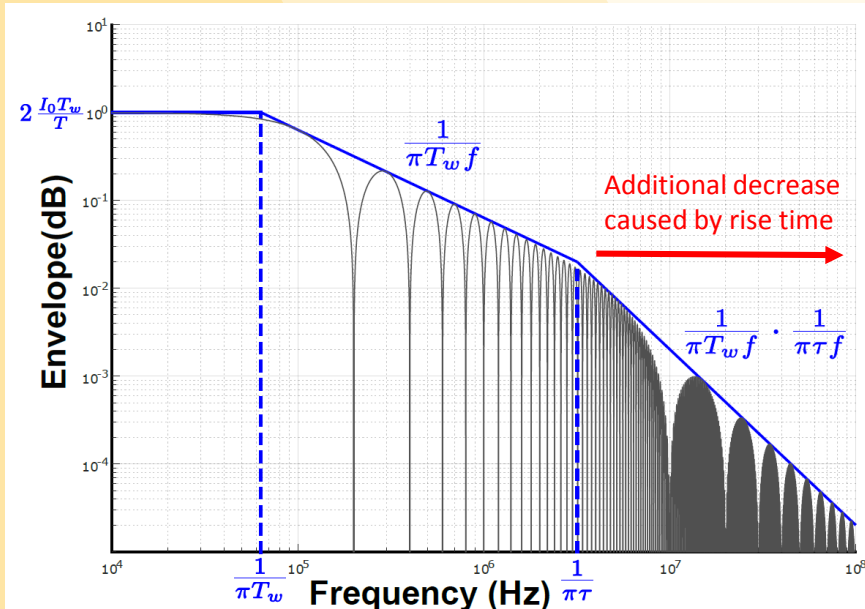
[Voltage response from a step current with different rise time]



[Impedance profile of the simplified PDN]

- : When rise time is short such as less than 2ns, the maximum voltage droops are almost same.
- : On the other hand, when rise time is long, the level of voltage droop decreases significantly.

- Fourier series expansion of trapezoidal current wave form



[Envelope of trapezoidal current in the frequency domain]

$$: i(t) = \frac{I_0 T_w}{T} \left(1 + 2 \sum_{n=1}^{\infty} \cdot \frac{\sin\left(\frac{n\pi T_w}{T}\right)}{\frac{n\pi T_w}{T}} \cdot \frac{\sin\left(\frac{n\pi\tau}{T}\right)}{\frac{n\pi\tau}{T}} \cdot \cos\left(\frac{2\pi n}{T}t\right) \right)$$

$$: Envelope(dB) = 2 \frac{I_0 T_w}{T} \left| \frac{\sin(\pi T_w f)}{\pi T_w f} \right| \left| \frac{\sin(\pi\tau f)}{\pi\tau f} \right|$$

: Previously, we consider Z_0 (characteristic impedance) at f_r (resonant frequency) to calculate the voltage droop from an ideal step current.

: The reduced magnitude of current harmonics needs to be applied for the voltage droop estimation.

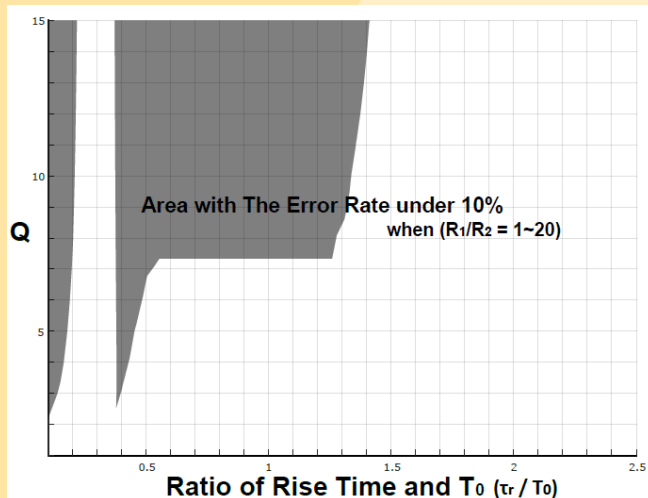
- Simplified equation to predict voltage droops

$$V_{step} = \frac{1}{\pi\tau f_r} \cdot Z_0 \cdot I_{step}$$

$$= \frac{1}{\pi\tau \cdot \frac{1}{2\pi\sqrt{LC}}} \cdot \sqrt{\frac{L}{C}} \cdot I_{step}$$

$$= \frac{2L}{\tau} \cdot I_{step} \quad (\text{when } f_r > \frac{1}{\pi\tau})$$

- Sufficient condition for equation's results



[Sufficient condition for the error rates under 10%]

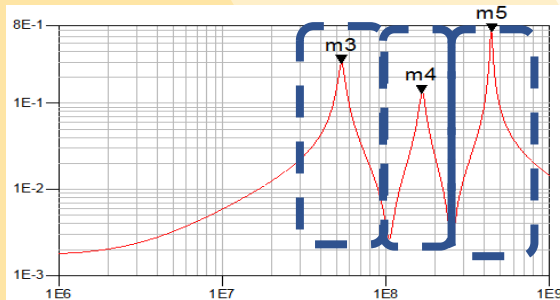
: Original equation can be used
when $Q > 8$ and $\tau < 0.1 \cdot T_0$

: New equation can be used
when $Q > 8$ and $0.4 \cdot T_0 < \tau < 1.2 \cdot T_0$

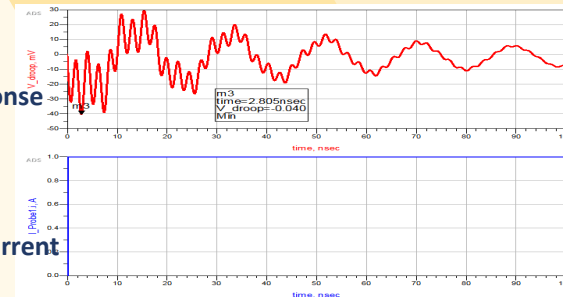
4.1 Ideal Step Current Response

- Goal

: Determine Max. Vol. droops from a step current with multiple peaks in impedance profile.

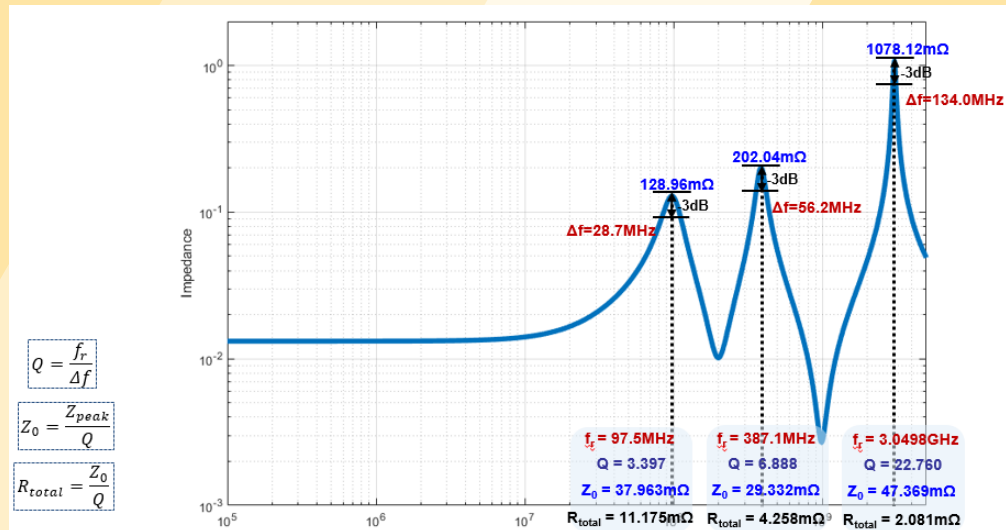


Step Response



Load Step current

- Variables required in impedance profile : Z_{peak} , w_0 , Q of each peak



→ Z_0 , w_0 , Q of each peak

$$Q = \frac{f_r}{\Delta f}$$

$$Z_0 = \frac{Z_{peak}}{Q}$$

$$R_{total} = \frac{Z_0}{Q}$$

4.1 Ideal Step Current Response

- Applying the equation with the variables from each peak

$$v(t)_{step} = \left[\frac{N}{N+1} \right] R_{total} - Z_0 \cdot e^{-\left(\frac{w_0}{2Q}\right)t} \cdot \left(Q - \frac{1}{Q} \frac{N}{(N+1)^2} \right) \cdot \cos(w_0 \cdot \sqrt{1 - \frac{1}{4Q^2}} t - \varphi)$$

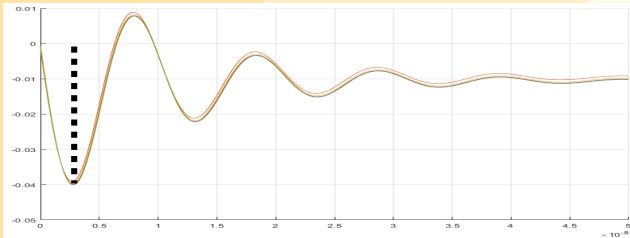
$$\varphi = \tan^{-1} \left[\frac{1}{2} + \frac{N^2}{(N+1)(1-N)} - Q^2 \frac{(1+N)}{(1-N)} \right] \cdot \sqrt{Q^2 - \frac{1}{4}}$$

Set $N_1, N_2, N_3 = 1 \sim 10$

Results

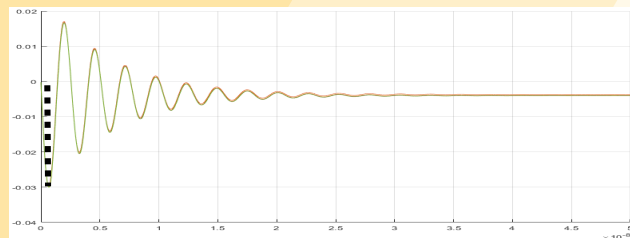
[1st peak]

$f_r = 97.5\text{MHz}$
 $Q = 3.397$
 $Z_0 = 37.963\text{m}\Omega$
 $R_{total} = 11.175\text{m}\Omega$



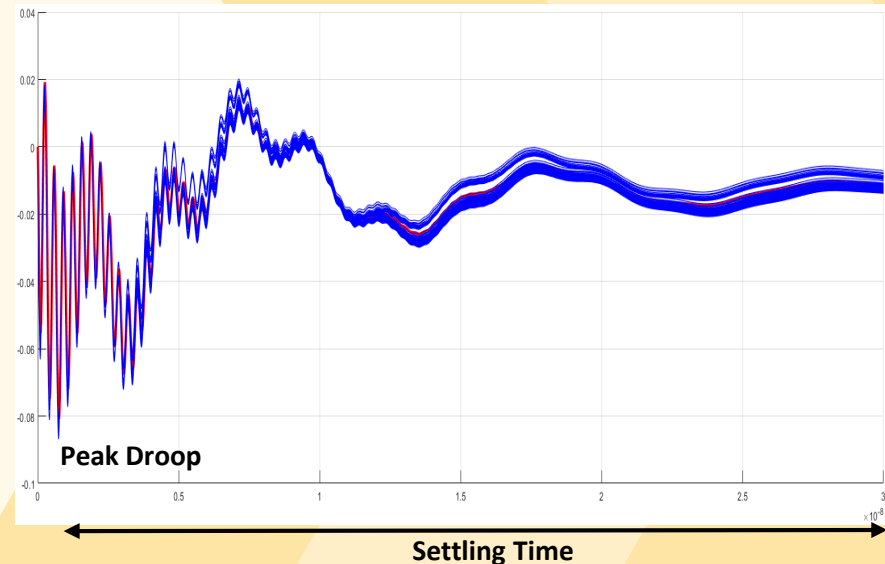
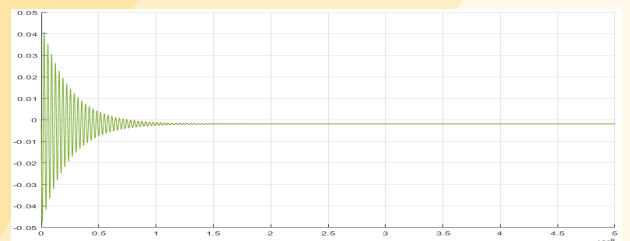
[2nd peak]

$f_r = 387.1\text{MHz}$
 $Q = 6.888$
 $Z_0 = 29.332\text{m}\Omega$
 $R_{total} = 4.258\text{m}\Omega$



[3rd peak]

$f_r = 3.0498\text{MHz}$
 $Q = 22.760$
 $Z_0 = 47.369\text{m}\Omega$
 $R_{total} = 2.081\text{m}\Omega$



[ADS]

Max. V : 80.8mV

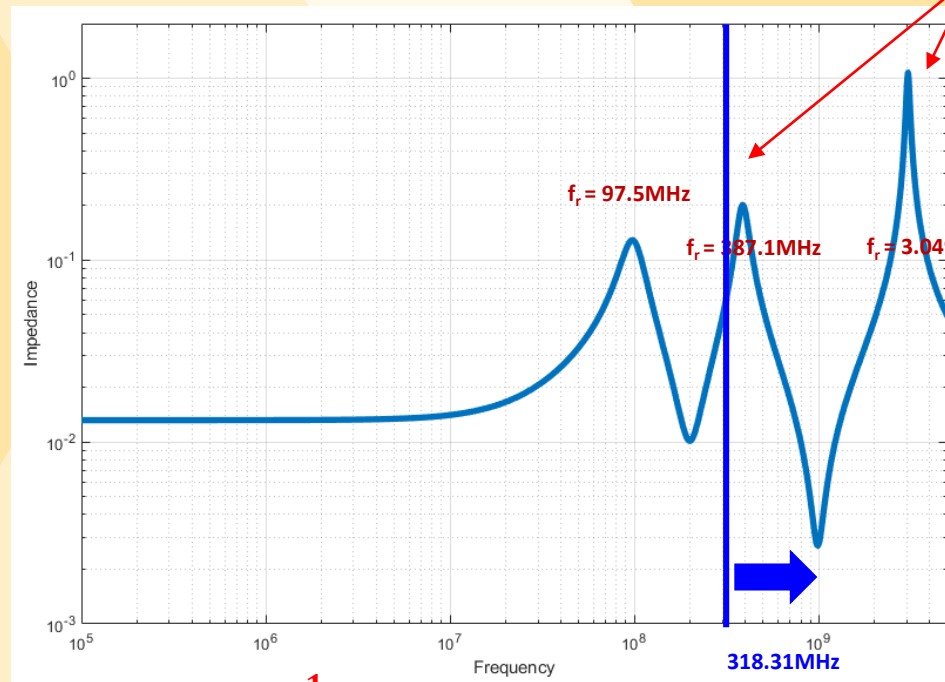
[This work]

Max. V : 80.31-86.89mV → Error : -0.6% ~ 7.01%

4.2 Step Current with Rise Time Response

- Consider rising time of step current τ_r
- : Apply **Envelop 1/x** for the peaks which Freq. is **over 1/(\pi\tau_r)**
- Case. : rise time 1ns

$$\frac{1}{\pi\tau_r} = 318.31\text{MHz}$$



$$v(t)_{step} = \frac{N}{N+1} R_{total} \underbrace{\frac{1}{\pi\tau_r f}}_{\text{Envelop}} \cdot Z_0 \cdot e^{-\left(\frac{\omega_0}{2Q}\right) \cdot t} \cdot \sqrt{\frac{\left(Q - \frac{1}{Q} \frac{N}{(N+1)^2}\right)^2}{Q^2 - \frac{1}{4}}} \cdot \cos(\omega_0 \cdot \sqrt{1 - \frac{1}{4Q^2}} t - \varphi)$$

4.2 Step Current with Rise Time Response

Results

- Rising time 500ps

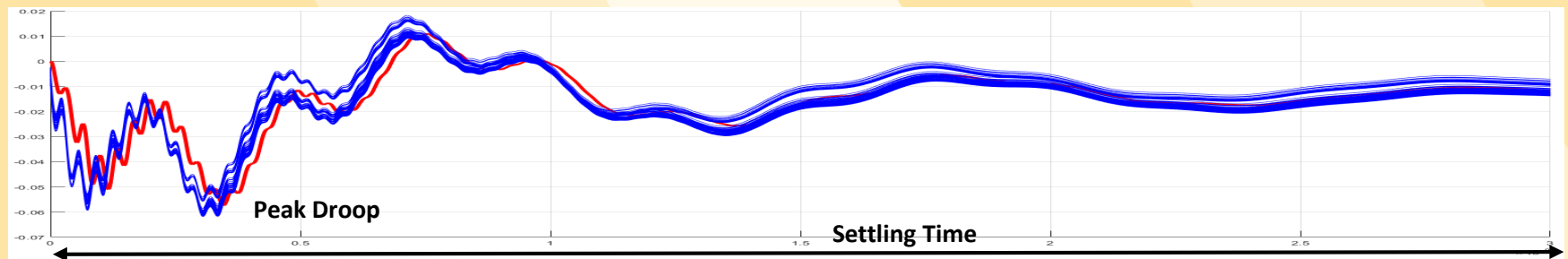
[ADS]

Max. V : 57.49mV

[This work]

Max. V : 54.17 – 61.87mV

→ Error : -5.77% ~ 7.62%



- Rising time 1ns

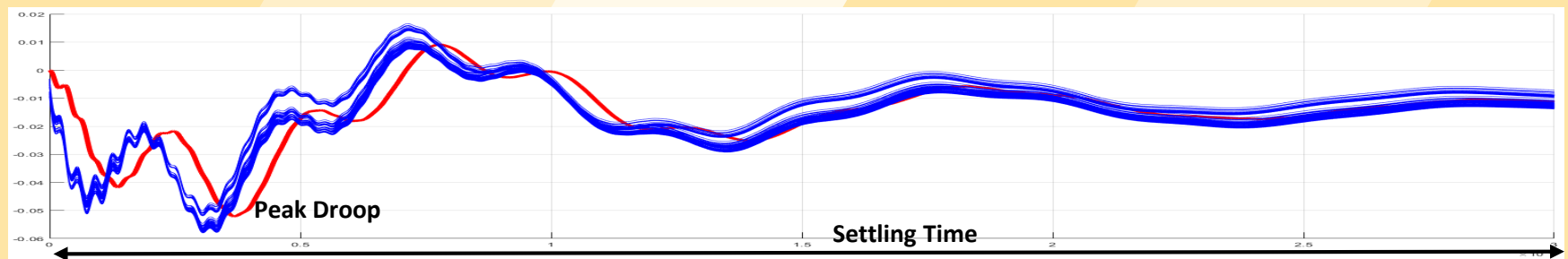
[ADS]

Max. V : 52.14mV

[This work]

Max. V : 50.11 – 58.02mV

→ Error : -3.98% ~ 11.28%



- Using the simplified equation, we can expect max. voltage droop from a step current with rise time.
- Utilizing the equation, we can estimate the voltage response waveform when multiple peaks existed.

Timeline

	19 4Q	19 1Q	19 2Q	19 3Q	19 3Q
Check Feasibility of ML usage with 1peak impedance					
Estimation of Vol. Multiple peaks impedance using ML					
Estimation of Vol. from arbitrary current using ML					