

Model of Axial Loading 1

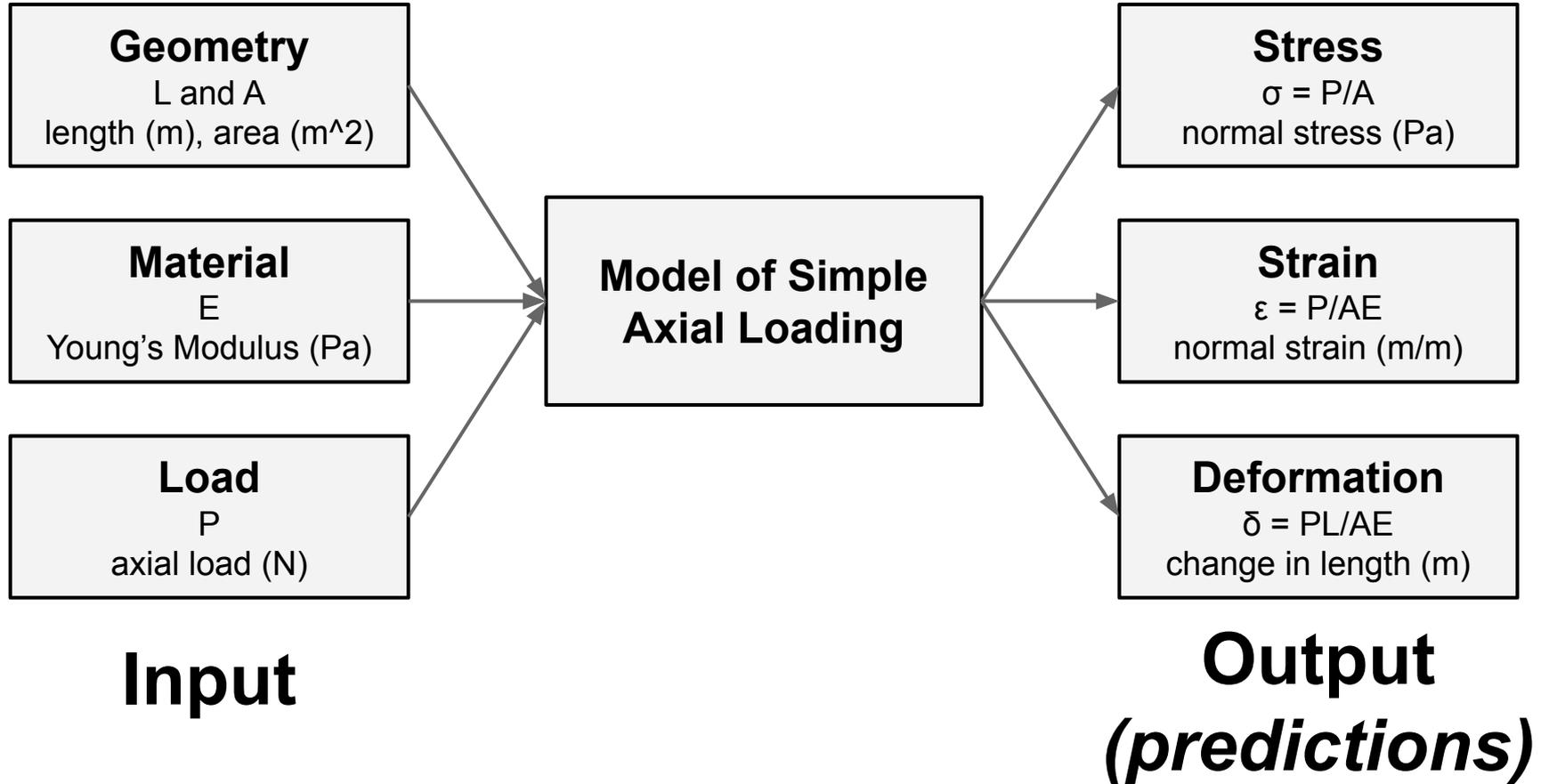
Prof. Charlie Kemp

BMED 3410: Introduction to Biomechanics
September 7, 2022
Lecture 5

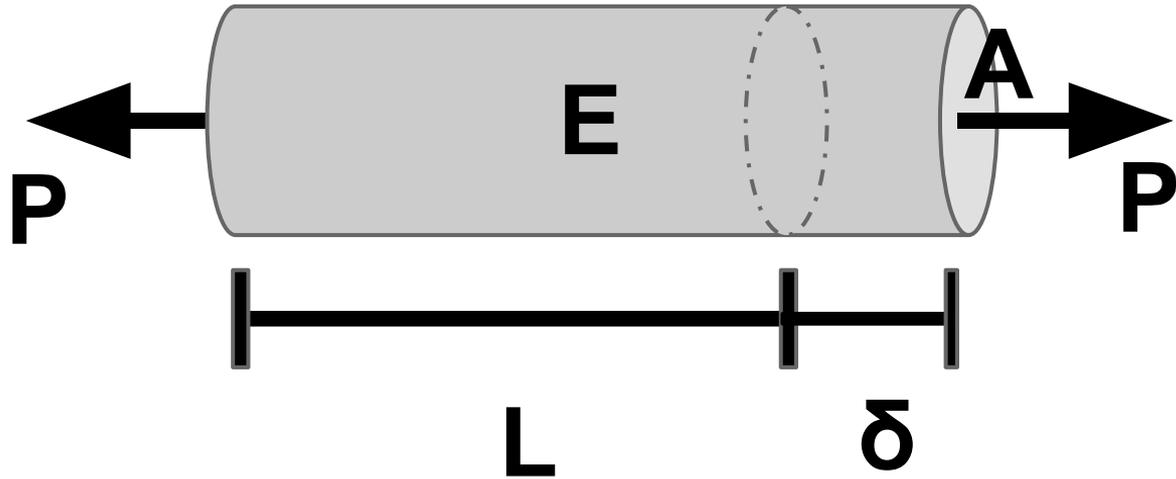
Outline

1. Material sample characterization wrap-up
 - a. <https://sites.gatech.edu/intro-to-biomechanics/>
2. Axial loading model with varying
 - a. Geometry
 - b. Material
 - c. Load
3. An example with graphs

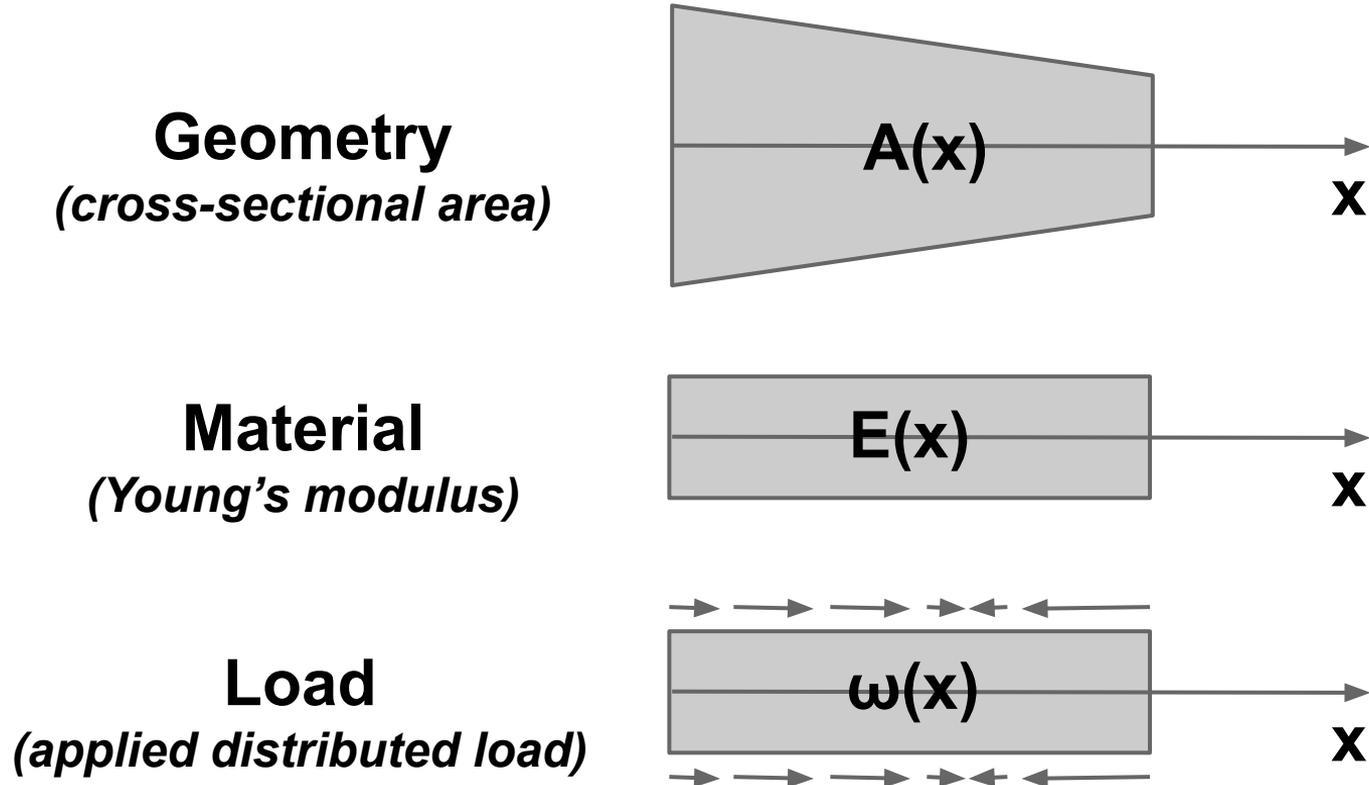
Model of Simple Axial Loading



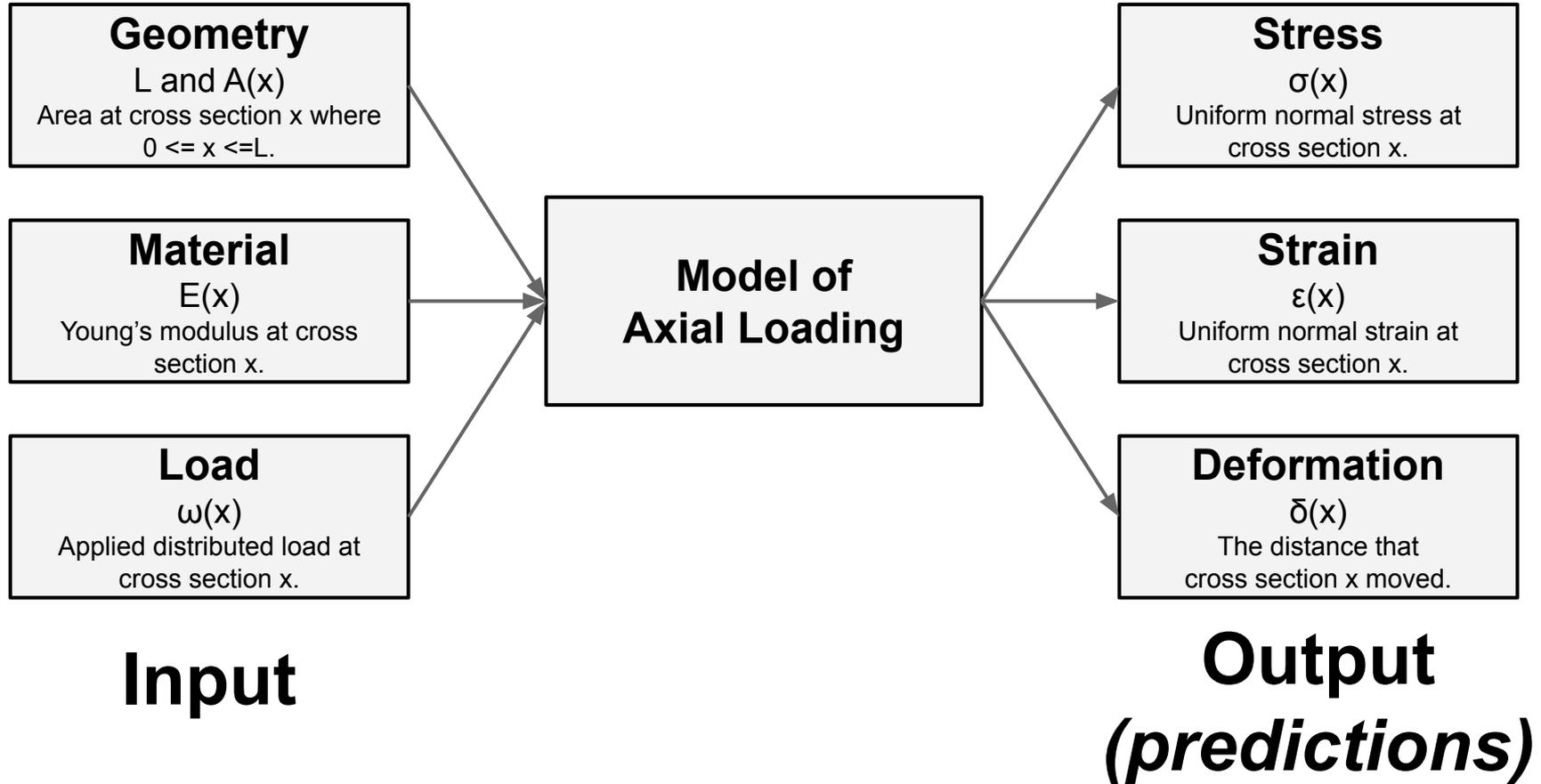
Model of Simple Axial Loading



Generalize the Model for Axial Variation in



Model of Axial Loading



Observe a Real Rubber Band

- Axially varying load ($\omega(x)$)
 - Predict change in the uniformly spaced markings on a rubber band when pulled at its two ends.
 - Predict change when load applied at the ends and the middle of the rubber band.
- Axially varying cross-sectional area ($A(x)$)
 - Predict change in the uniformly spaced markings on a rubber band that has been cut to be narrow in the middle when pulled at its two ends.
 - Predict where the rubber band that has been cut to be narrow in the middle will fail.
- Axially varying material ($E(x)$)
 - Predict what happens when the rubber band is connected in series with a paperclip.

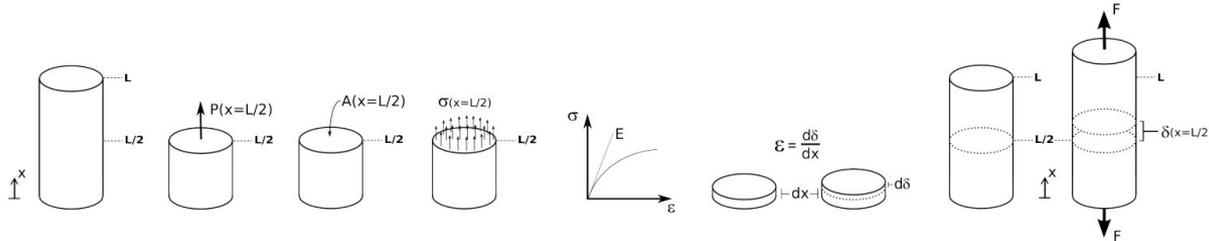
BMED 3400 Axial Loading Chart

version 1.1

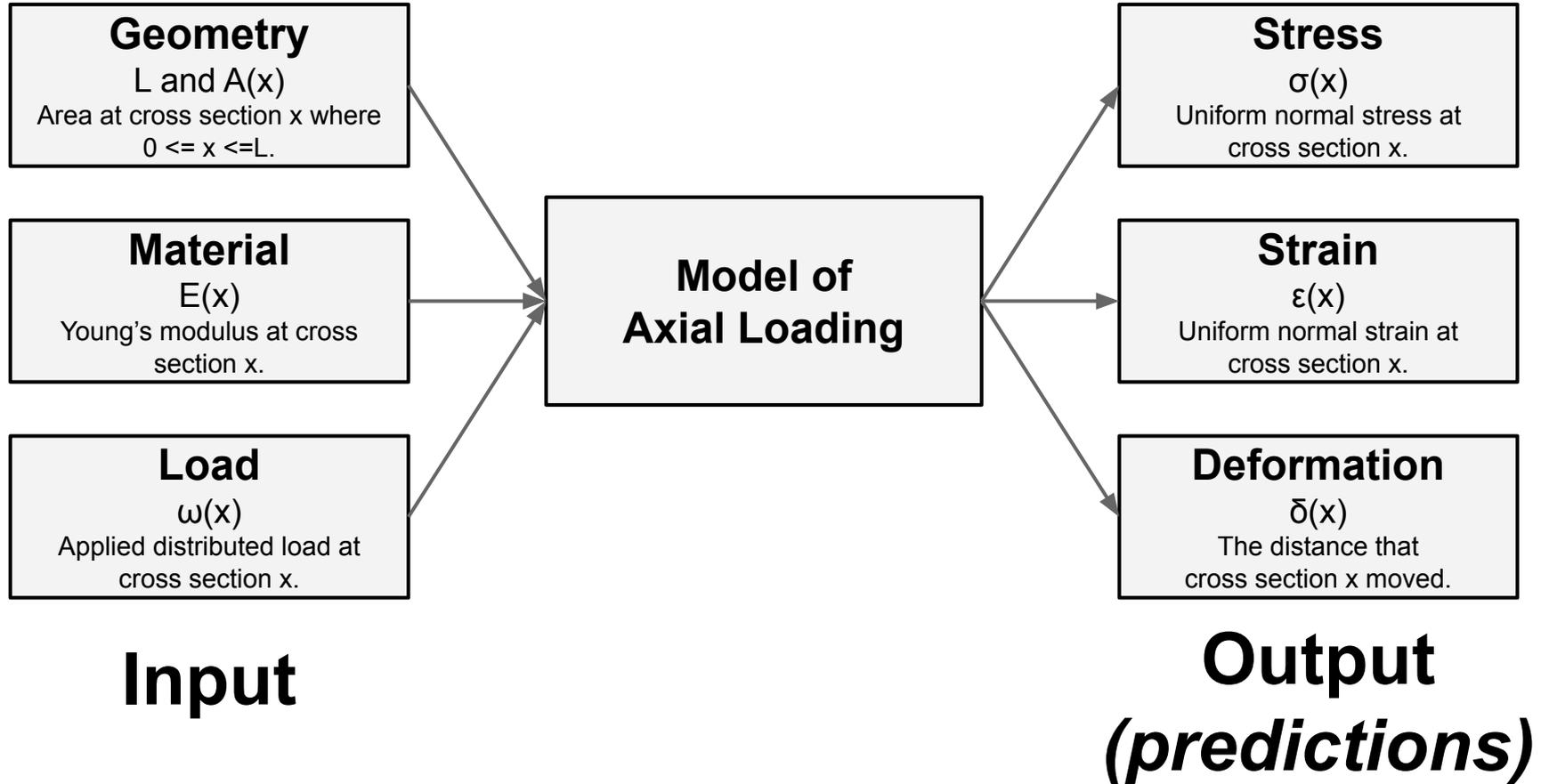
Prof. Charles C. Kemp, PhD

January 26, 2016

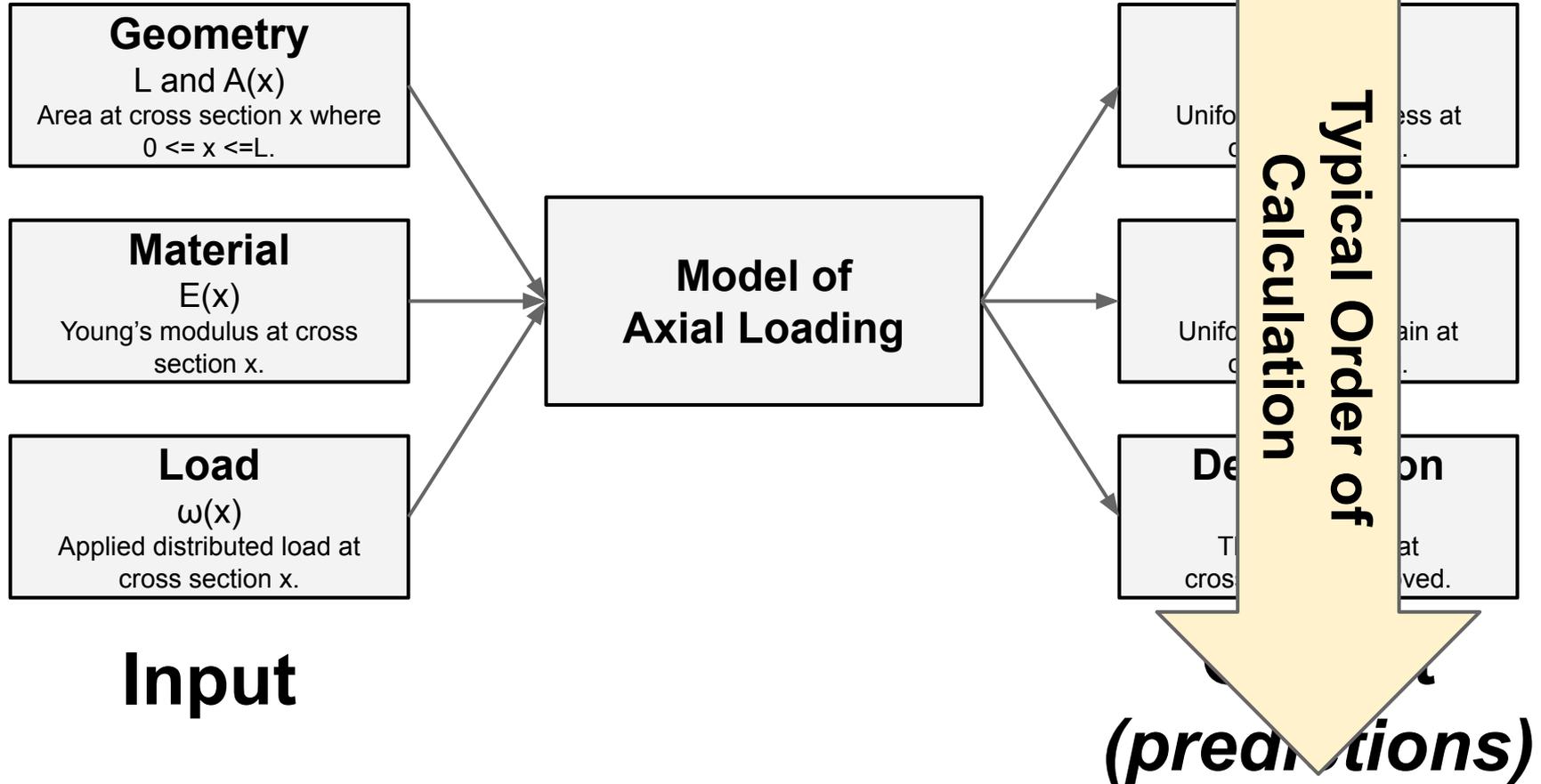
variable	units	relationship to other variables	name	description
L	meters, m		length of the object	length of axially loaded non-rigid object; model tends to work better for long narrow objects
x	meters, m	$0 \leq x \leq L$	location of a cross-section	location of cross section along length of object prior to loading; cross section is normal to axis of object
$\omega(x)$	$\frac{N}{m}$	$\int_{-x}^{L+x} \omega(x) dx = 0$ due to static equilibrium	applied distributed load	applied load points in $+x$ direction $\Rightarrow \omega(x) < 0$; applied load points in $-x$ direction $\Rightarrow \omega(x) > 0$
$P(x)$	newtons, N	$P(x) = \int_{-x}^x \omega(\alpha) d\alpha = -\int_x^{L+x} \omega(\alpha) d\alpha$	internal axial load	total internal force normal to cross section at x ; $P > 0$ if cross-sectional sliver of length dx is in tension
$A(x)$	m^2	$A(x) = \int_{\text{cross-section}(x)} 1 dA$	cross-sectional area	area of cross section at x
$\sigma(x)$	pascals, $\frac{N}{m^2}$	$\sigma(x) = \frac{P(x)}{A(x)}$, $\sigma = \frac{dF}{dA}$, $P(x) = \int_{A(x)} \sigma(x) dA$	normal stress	average normal stress across the cross section at x ; uniform stress model; $\sigma > 0$ when in tension
$E(x)$	pascals, $\frac{N}{m^2}$	$E(x) = \frac{P(x)}{\epsilon(x)}$	Young's modulus	model of the material; slope of linear approximation to stress-strain curve at 0,0; stiffness of the material
$\epsilon(x)$	unitless, %, $\frac{m}{m}$	$\epsilon(x) = \frac{\sigma(x)}{E(x)}$, $\epsilon(x) = \frac{P(x)}{E(x)A(x)}$, $\epsilon = \frac{d\delta}{dx}$	normal strain	% change in length of cross-sectional sliver of length dx located at x ; $\epsilon > 0$ represents length increase
$\delta(x)$	meters, m	$\delta(x) = \int_{-x}^x \epsilon(\alpha) d\alpha$, $\delta_{total} = \delta(L)$, $\delta(0) = 0$	deformation	distance cross section at x displaces due to load; $\delta = 0 \Rightarrow$ no change; $\delta > 0 \Rightarrow$ displaced in positive x direction



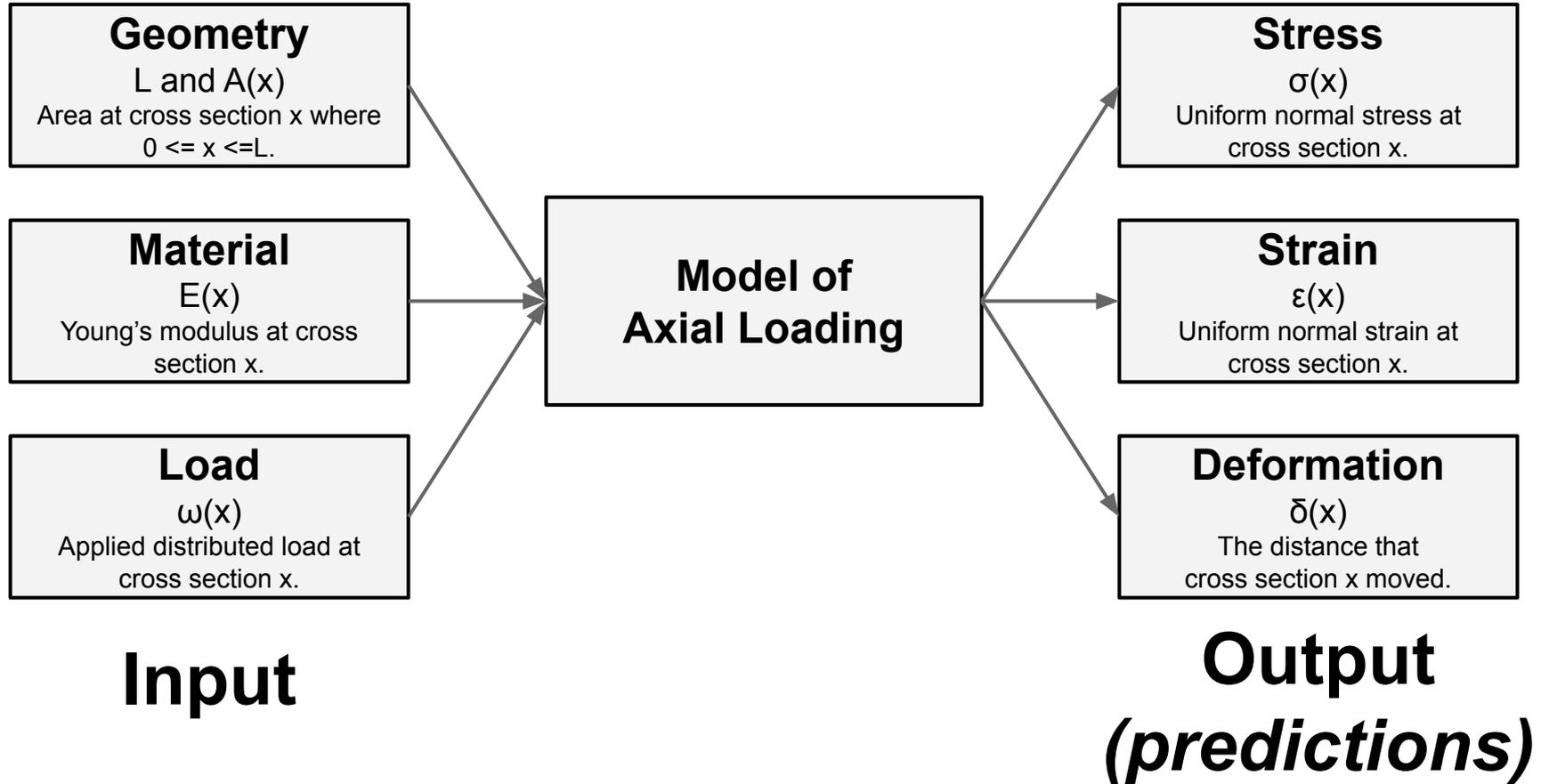
Model of Axial Loading



Model of Axial Loading



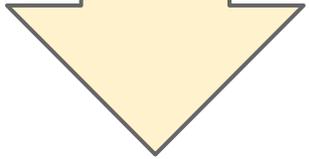
Model of Axial Loading



<i>variable</i>	<i>units</i>	<i>relationship to other variables</i>	<i>name</i>
L	meters, m		length of the object
x	meters, m	$0 \leq x \leq L$	location of a cross-section
$\omega(x)$	$\frac{N}{m}$	$\int_{-\epsilon}^{L+\epsilon} \omega(x) dx = 0$ due to static equilibrium	applied distributed load
$P(x)$	newtons, N	$P(x) = \int_{-\epsilon}^x \omega(\alpha) d\alpha = -\int_x^{L+\epsilon} \omega(\alpha) d\alpha$	internal axial load
$A(x)$	m^2	$A(x) = \int_{shape(x)} 1 dA$	cross-sectional area
$\sigma(x)$	pascals, $\frac{N}{m^2}$	$\sigma(x) = \frac{P(x)}{A(x)}$, $\sigma = \frac{dF}{dA}$, $P(x) = \int_{A(x)} \sigma(x) dA$	normal stress
$E(x)$	pascals, $\frac{N}{m^2}$	$E(x) = \frac{\sigma(x)}{\varepsilon(x)}$	Young's modulus
$\varepsilon(x)$	unitless, %, $\frac{m}{m}$	$\varepsilon(x) = \frac{\sigma(x)}{E(x)}$, $\varepsilon(x) = \frac{P(x)}{E(x)A(x)}$, $\varepsilon = \frac{d\delta}{dx}$	normal strain
$\delta(x)$	meters, m	$\delta(x) = \int_{-\epsilon}^x \varepsilon(\alpha) d\alpha$, $\delta_{total} = \delta(L)$, $\delta(0) = 0$	deformation

v	<i>units</i>	<i>relationship to other variables</i>	<i>name</i>
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	meters, m	$\delta(x) = \int_{-\epsilon}^x \epsilon(\alpha) d\alpha$, $\delta_{total} = \delta(L)$, $\delta(0) = 0$	deformation

Typical Order of Calculation

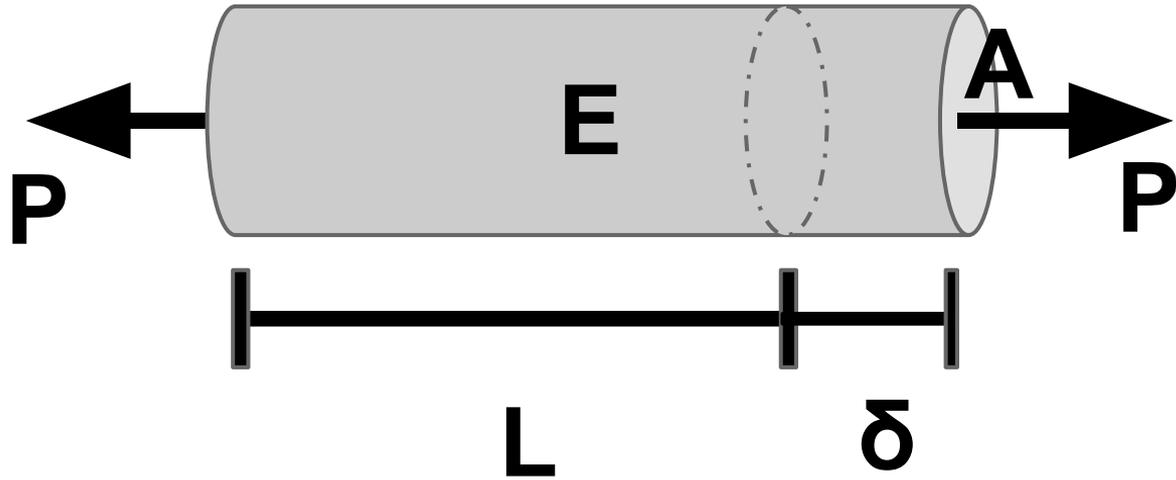


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$A(x)$	m^2	$A(x) = \int_{shape(x)} 1 dA$	cross-sectional area
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$E(x)$	pascals, $\frac{N}{m^2}$	$E(x) = \frac{\sigma(x)}{\varepsilon(x)}$	Young's modulus
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$\delta(x)$	meters, m	$\delta(x) = \int_{-\epsilon}^x \varepsilon(\alpha) d\alpha$, $\delta_{total} = \delta(L)$, $\delta(0) = 0$	deformation

Use Piecewise Low-order Polynomial Functions

- Use piecewise polynomial functions to quickly create models and graph key quantities
- <http://en.wikipedia.org/wiki/Piecewise>
- Generate the functions by integrating
 - dirac delta
 - constant
 - linear
 - quadratic
 - ...
- Draw graphs instead of integrating with symbols

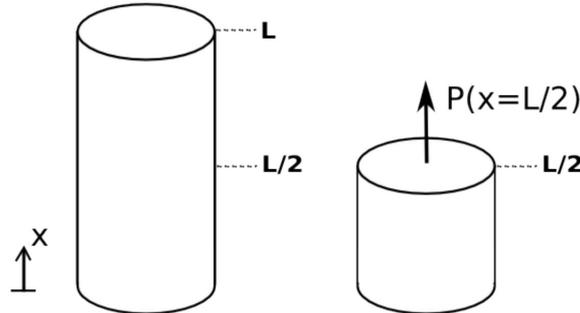
Example #1

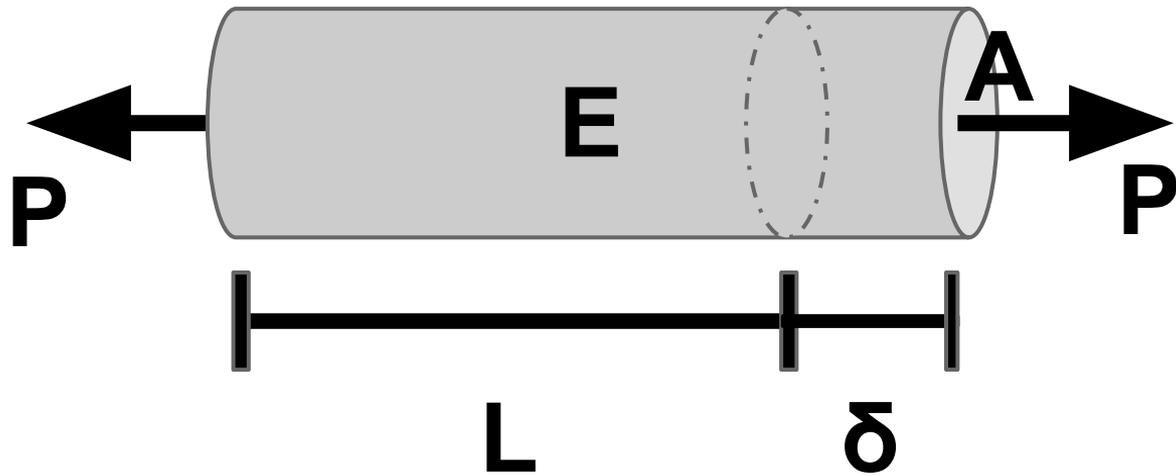


From Applied Distributed Load to the Internal Axial Load

- $\omega(x)$ represents the applied distributed load
- integrate it to find the internal axial load, $P(x)$

$\omega(x)$	$\frac{N}{m}$	$\int_{-\epsilon}^{L+\epsilon} \omega(x) dx = 0$ due to static equilibrium
$P(x)$	newtons, N	$P(x) = \int_{-\epsilon}^x \omega(\alpha) d\alpha = - \int_x^{L+\epsilon} \omega(\alpha) d\alpha$





How can we represent a concentrated load with a distribution?

- Dirac delta function

- “The Dirac delta can be loosely thought of as a function on the real line which is zero everywhere except at the origin, where it is infinite,”

Not deformation! 

$$\delta(x) = \begin{cases} +\infty, & x = 0 \\ 0, & x \neq 0 \end{cases}$$

- “and which is also constrained to satisfy the identity”

$$\int_{-\infty}^{\infty} \delta(x) dx = 1$$

More About the Dirac Delta Function

“integration of the delta function results in the [Heaviside step function](#)”

$$H(x) := \int_{-\infty}^x \delta(s) ds$$

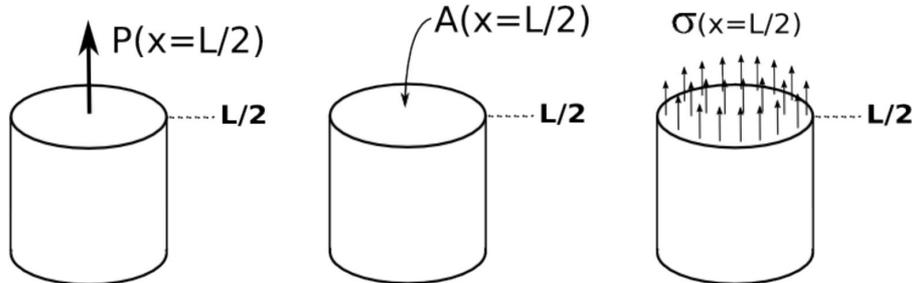
“The [distributional derivative](#) of the [Heaviside step function](#) is the [Dirac delta function](#)”

$$\frac{dH(x)}{dx} = \delta(x)$$

From Internal Axial Load to Stress

- To find stress, $\sigma(x)$, simply divide the internal axial load, $P(x)$, by the area, $A(x)$.

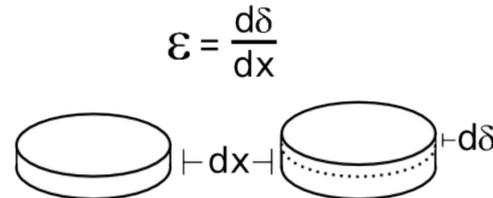
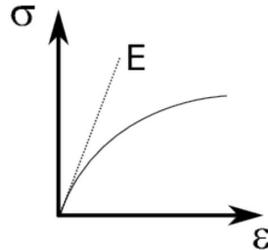
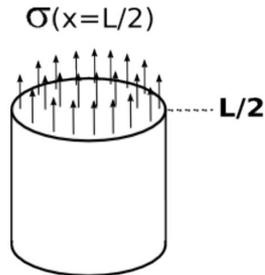
$P(x)$	newtons, N	$P(x) = \int_{-\epsilon}^x \omega(\alpha) d\alpha = - \int_x^{L+\epsilon} \omega(\alpha) d\alpha$
$A(x)$	m^2	$A(x) = \int_{shape(x)} 1 dA$
$\sigma(x)$	pascals, $\frac{N}{m^2}$	$\sigma(x) = \frac{P(x)}{A(x)}$, $\sigma = \frac{dF}{dA}$, $P(x) = \int_{A(x)} \sigma(x) dA$



From Stress to Strain

- To find strain, $\varepsilon(x)$, simply divide stress, $\sigma(x)$, by Young's modulus, $E(x)$.

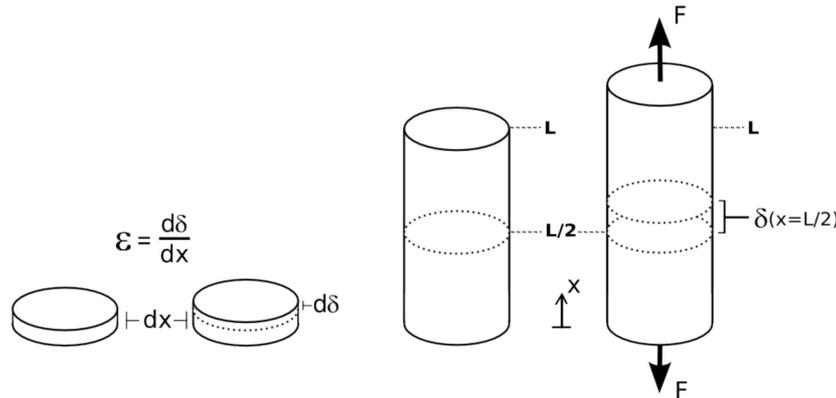
$\sigma(x)$	pascals, $\frac{N}{m^2}$	$\sigma(x) = \frac{P(x)}{A(x)}$, $\sigma = \frac{dF}{dA}$, $P(x) = \int_{A(x)} \sigma(x) dA$
$E(x)$	pascals, $\frac{N}{m^2}$	$E(x) = \frac{\sigma(x)}{\varepsilon(x)}$
$\varepsilon(x)$	unitless, %, $\frac{m}{m}$	$\varepsilon(x) = \frac{\sigma(x)}{E(x)}$, $\varepsilon(x) = \frac{P(x)}{E(x)A(x)}$, $\varepsilon = \frac{d\delta}{dx}$



From Strain to Deformation

- Integrate the strain, $\epsilon(x)$, to find how far the cross section at x has moved, $\delta(x)$.

$\epsilon(x)$	unitless, %, $\frac{m}{m}$	$\epsilon(x) = \frac{\sigma(x)}{E(x)}$, $\epsilon(x) = \frac{P(x)}{E(x)A(x)}$, $\epsilon = \frac{d\delta}{dx}$
$\delta(x)$	meters, m	$\delta(x) = \int_{-\epsilon}^x \epsilon(\alpha) d\alpha$, $\delta_{total} = \delta(L)$, $\delta(0) = 0$



$\varepsilon(x)$	unitless, %, $\frac{m}{m}$	$\varepsilon(x) = \frac{\sigma(x)}{E(x)}$, $\varepsilon(x) = \frac{P(x)}{E(x)A(x)}$, $\varepsilon = \frac{d\delta}{dx}$
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